

# TITLE OF THE INVENTION

OPTICAL ENCODER AND OUTPUT ADJUSTMENT FOR THE SAME  
CROSS-REFERENCE TO RELATED APPLICATIONS

This application is based upon and claims the  
5 benefit of priority from the prior Japanese Patent  
Application No. 2003-030875, filed February 7, 2003,  
the entire contents of which are incorporated herein by  
reference.

## BACKGROUND OF THE INVENTION

### 10 1. Field of the Invention

The present invention relates to an optical  
encoder and a method of adjusting its output signal  
level.

### 2. Description of the Related Art

15 Encoders are used for detecting displacement in  
the linear direction in machine tool stages and  
three-dimensional measuring instruments. Optical and  
magnetic encoders are also used for detecting  
a rotational angle of servo motors and the like.

20 An optical encoder is generally composed of  
a scale fixed to a member for detecting displacement of  
a stage or the like, and a sensor head for detecting  
displacement of the scale. The sensor head includes  
a light source for emitting light to the scale, and a  
25 light detector for detecting a light beam transmitted,  
reflected or diffracted from the scale, and the  
movement of the scale is detected by change of the

received light signal.

As a prior art, a representative optical encoder is explained by referring to FIG. 23. FIG. 23 is a block diagram showing a laser encoder of a prior art using a surface-emitting laser and a reflection type scale.

Such a laser encoder using a surface-emitting laser and a reflection type scale is disclosed, for example, in Jpn. Pat. Appln. KOKAI Publication No. 2002-48602.

This encoder is composed of a reflection type scale 20 and a sensor head 30 as shown in FIG. 23. An optical pattern 23 for detecting a moving distance is formed on a surface of the scale 20, and this pattern is made by patterning a member of high reflectivity made of an aluminum or the like on a surface of a transparent member of glass or the like. The sensor head 30 has a light detector 37 for detecting the moving distance formed on a semiconductor substrate 34, and a coherent light source (hereinafter called light source) 321 for detecting the moving distance disposed on the semiconductor substrate 34. The relative positional relation of the light source 321 and the light detector 37 is kept constant.

The scale 20 cooperates with a stage (not shown), and moves in the arrow direction in FIG. 23 relatively to the sensor head 30, and the sensor head 30 detects

its moving distance by the change of intensity of  
a diffracted light from the scale 20. The detection  
signal of the moving distance is produced as a waveform  
as shown, for example, in FIG. 24. Herein, phase A and  
5 phase B are waveforms produced along with the movement  
of the scale 20, are generally quasi sinusoidal waves.  
Phase A and phase B are outputs different in phase by  
90 degrees, and from the relation in phase of signals  
of phase A and phase B, the moving direction of the  
10 scale 20 can be detected. The scale 20 changes its  
position while maintaining a positional relation  
capable of forming a so-called Talbot image relatively  
to the sensor head 30.

The Talbot image is explained by referring to  
15 FIG. 25. For the sake of simplicity of explanation,  
a transmission type encoder is assumed, and it is  
discussed same also in a reflection type encoder.

As shown in FIG. 25, parameters are defined as  
follows:

20 z1 is a distance between a light source 1 and  
a surface of a scale 2 having diffraction grating  
formed thereon;

z2 is a distance between the surface on the scale  
2 having the diffraction grating formed thereon and  
25 a light detector 3;

p1 is a pitch of the diffraction grating on the  
scale 2; and

p2 is a pitch of a diffraction interference pattern on a receiving surface of the light detector 3.

The "pitch of the diffraction grating on the scale 2" is a spatial period of an optical pattern modulated in optical characteristic and formed on the scale 2.

The "pitch of a diffraction interference pattern on a receiving surface of the light detector 3" is a spatial period of an intensity distribution (light intensity pattern) of the diffraction pattern formed on the receiving surface.

According to the diffraction theory of light, when the z1 and z2 defined above are in a specific relation satisfying the relation represented by the following formula (1), a light intensity pattern similar to the diffraction grating pattern of the scale 2, or so-called Talbot image, is formed on the receiving surface of the light detector 3:

$$(1/z1) + (1/z2) = \lambda / (k(p1)^2) \quad (1)$$

where  $\lambda$  is a wavelength of a light beam emitted from the light source 1; and k is a natural number.

At this time, the pitch p2 of the diffraction interference pattern on the receiving surface can be expressed by the following formula (2):

$$P2 = p1 \times (z1 + z2)/z1 \quad (2)$$

When the scale 2 displaces in the pitch direction of the diffraction grating relatively to the light source 1, the light intensity pattern of the

diffraction interference pattern is moved in the dislocating direction of the scale 2 while keeping the same spatial period.

Therefore, when a spatial period  $p_{20}$  of the photo  
5 detector 4 of the light detector 3 is set in the same value as  $p_2$ , every time the scale 2 moves in the pitch direction by distance of  $p_1$ , a periodic intensity signal is obtained from the light detector 3, so that the displacement of the scale 2 in the pitch direction  
10 can be detected.

Back to FIG. 23, the light source 321 for detecting the moving distance, the optical pattern 23 for detecting the moving distance, and the photo  
15 detector of the light detector 37 are disposed in a positional relation capable of forming the Talbot image, and a light and dark pattern similar to the optical pattern 23 for detecting the moving distance formed on the scale 20 is projected on the photo  
20 detector of the light detector 37. The period of this light and dark pattern is the period  $p_2$  calculated by the formula (2). The photo detector on the light detector 37 is formed to have this period of  $p_2$ , and with this photo detector, the movement of the light and dark pattern can be detected.

25 Since the optical encoder is high precision, high resolution, and contact-free type, and is excellent in electromagnetic wave interference tolerance,

the optical encoder is used in wide fields, and in particular the optical type is in the mainstream in encoders demanding high precision and high resolution.

#### BRIEF SUMMARY OF THE INVENTION

5           The first phase of the present invention relates to an optical encoder comprising:

          a light source unit;

          a scale which has a periodic optical pattern and displaces relatively to the light source unit; and

10           a light detector to detect a light beam emitted from a light source of the light source unit and traveled by way of the scale;

          wherein the light source unit has a light beam exit opening through which a light beam is emitted  
15           toward the scale, and

          assuming that a distance between the light beam exit opening and the scale is  $z_1$ , a distance between the scale and the light detector is  $z_2$ , and a pitch of the periodic optical pattern of the scale is  $p_1$ , the  
20           width  $W$  of the light beam exit opening in a scale moving direction is determined depending on the values of  $z_1$ ,  $z_2$ , and  $p_1$ .

          The second phase of the present invention relates to the optical encoder according to the first phase,  
25           wherein the width  $W$  of the light beam exit opening in the scale moving direction is specified preferably as follows:

$$p_1 \times (2n - 1.5) \times (z_1 + z_2) / (2 \times z_2) \leq W \leq p_1 \times (2n - 0.5) \times (z_1 + z_2) / (2 \times z_2)$$

where n is a natural number.

5 The third phase of the present invention relates to the optical encoder according to the second phase, wherein the width W of the light beam exit opening in the scale moving direction is preferably represented approximately as follows:

$$p_1 \times (2n-1) \times (z_1 + z_2) / (2 \times z_2).$$

10 The fourth phase of the present invention relates to the optical encoder according to the second phase, wherein the values of  $z_1$  and  $z_2$  are preferably substantially equal to each other.

15 The fifth phase of the present invention relates to the optical encoder according to the second phase, wherein one or more light beam exit openings are disposed in the scale moving direction preferably at a position of  $(z_1 + z_2) / z_2 \times m$  (where m is a natural number) times of the pitch  $p_1$  of the periodic optical  
20 pattern of the scale.

1 The sixth phase of the present invention relates to the fifth phase, wherein the light beam exit opening of the light source unit is preferably a light beam exit window formed on a light beam emission surface of  
25 the light source, and the width W of the light beam exit opening in the scale moving direction is the width  $W_L$  of the light beam exit window in the scale moving

direction.

The seventh phase of the present invention relates to the optical encoder according to the fifth phase, wherein the light beam exit opening of the light source unit is preferably an optical element disposed on an optical path of a light beam from the light source toward the scale and transmitting a predetermined portion of the light beam.

The eighth phase of the present invention relates to the optical encoder according to the seventh phase, wherein the light beam exit opening of the light source unit, the scale, and the light detector are arranged preferably in a predetermined relation capable of detecting a Talbot image.

The ninth phase of the present invention relates to the optical encoder according to the seventh phase, wherein the optical encoder is configured preferably to satisfy approximately the relation of  $1/z_1 + 1/z_2 = \lambda / (n(p_1)^2)$ , where  $\lambda$  is a wavelength of the light beam emitted from the light beam exit opening; and  $n$  is a natural number.

The tenth phase of the present invention relates to the optical encoder according to the seventh phase, wherein the optical element transmitting the predetermined portion of the light beam is preferably a slit having a light transmitting portion and a light shielding portion, and the width  $W$  of the light beam



exit opening in the scale moving direction is the width  $W_s$  of the slit in the scale moving direction.

The eleventh phase of the present invention relates to the optical encoder according to the tenth phase, wherein the slit has preferably a plurality of openings in the scale moving direction, and the plurality of openings are disposed at positions of about integer times of the pitch  $p_2$  of the light detector.

The twelfth phase of the present invention relates to optical encoder according to the seventh phase, wherein the optical element transmitting the predetermined portion of the light beam is preferably a slit having a circular opening, and the width  $W$  of the light beam exit opening in the scale moving direction is a diameter  $W_s$  of the circular opening.

The thirteenth phase of the present invention relates to the optical encoder according to the twelfth phase, wherein the circular opening is plural, and the plurality of circular openings are disposed preferably at a position of about integer times of the pitch  $p_2$  of the light detector in the scale moving direction.

The fourteenth phase of the present invention relates to the optical encoder according to the thirteenth phase, wherein the circular opening is plural, and the plurality of circular openings are disposed preferably in a plane parallel to a pattern

surface of the scale, in a direction orthogonal to the scale moving direction.

The fifteenth phase of the present invention relates to the optical encoder according to the tenth phase, wherein the light source unit further has preferably a lens which sets a beam divergent angle of the light beam to a predetermined value.

The sixteenth phase of the present invention relates to the optical encoder according to the tenth phase, wherein the optical element transmitting the predetermined portion of the light beam is disposed preferably such that the light beam emitted from the light source unit is reflected by the scale, and then does not shield an optical path from the scale toward a region of the light detector having an effective reception sensitivity.

The seventeenth phase of the present invention relates to the optical encoder according to the tenth phase, further comprising preferably a plurality of photo detectors which detect a predetermined phase portion of a light intensity pattern on a receiving surface of the light detector formed when the light beam emitted from the light source unit and passing through the scale impinges upon the receiving surface.

The eighteenth phase of the present invention relates to the optical encoder according to the tenth phase, the photo detectors of the light detector is

configured preferably to be capable of detecting a predetermined phase portion of a light intensity pattern having a pitch of about  $p_1 \times (z_1 + z_2)/z_1$ .

5 The nineteenth phase of the present invention relates to the optical encoder according to the first phase, wherein the width  $W$  of the light beam exit opening in the scale moving direction is preferably  $p_1 \times (z_1 + z_2)/(2 \times z_2)$  or less.

10 The twentieth phase of the present invention relates to the optical encoder according to the nineteenth phase, wherein one or more light beam exit openings are disposed preferably in the scale moving direction at positions of  $(z_1 + z_2)/z_2 \times m$  (where  $m$  is an integer of 1 or more) times of the pitch  $p_1$  of the  
15 periodic optical pattern of the scale.

The twenty first phase of the present invention relates to the optical encoder according to the twentieth phase, wherein the light beam exit opening of the light source unit is preferably a light beam exit  
20 window formed on a light beam emission surface of the light source, and the width  $W$  of the light beam exit opening in the scale moving direction is the width  $W_L$  of the light beam exit window in the scale moving direction.

25 The twenty second phase of the present invention relates to the optical encoder according to the twentieth phase, wherein the light beam exit opening of

the light source unit is preferably an optical element disposed on an optical path of a light beam from the light source toward the scale and passing through a predetermined portion of the light beam.

5           The twenty third phase of the present invention relates to the optical encoder according to the twenty second phase, wherein the light beam exit opening of the light source unit, the scale, and the light detector are arranged preferably in a predetermined  
10           relation capable of detecting a Talbot image.

          The twenty fourth phase of the present invention relates to the optical encoder according to the twenty second phase, wherein the optical encoder is configured preferably to satisfy approximately the relation of  
15            $1/z_1 + 1/z_2 = \lambda / (n(p_1)^2)$ , where  $\lambda$  is a wavelength of the light beam emitted from the light beam exit opening and  $n$  is a natural number.

          The twenty fifth phase of the present invention relates to the optical encoder according to the twenty  
20           second phase, wherein the optical element transmitting the predetermined portion of the light beam is preferably a slit having a light transmitting portion and a light shielding portion, and the width  $W$  of the light beam exit opening in the scale moving direction  
25           is the width  $W_s$  of the slit in the scale moving direction.

          The twenty sixth phase of the present invention

relates to a method of adjusting an output signal level depending on a period  $p_2$  of a light intensity pattern formed on a receiving surface of a light detector, in an optical encoder comprising: a light source unit; an  
5 optical element of the light source unit, which causes a predetermined portion of a light beam emitted from a light source to pass therethrough; a scale which has a periodic optical pattern and displaces relatively to the light source unit; and a light detector to detect  
10 a light beam emitted from the light source unit and traveled by way of the scale, the method comprising:

(i) a step of detecting a light intensity pattern formed on the receiving surface of the light detector;

(ii) a step of checking a level of the output  
15 signal depending on the period  $p_2$  of the light intensity pattern detected by the light detector;

(iii) a step of determining whether or not the level of the output signal is included in a predetermined range; and

(iv) a step of, when the level of the output  
20 signal is not included in the predetermined range of the signal level, changing a distance from the optical element to the scale,

wherein the steps from (i) to (iv) are repeated to  
25 adjust the output signal level.

The twenty seventh phase of the present invention relates to an optical encoder comprising:

a light source unit;

a scale which has a periodic optical pattern and dislocates relatively to the light source unit; and

a light detector to detect a light beam emitted  
5 from the light source unit and traveled by way of the scale,

wherein the light source unit has an optical unit which sets a beam divergent angle of the light beam to a predetermined value.

10 The twenty eighth phase of the present invention relates to the optical encoder according to the twenty seventh phase, wherein the light source unit, the scale, and the light detector are arranged preferably in a predetermined relation capable of detecting  
15 a Talbot image.

The twenty ninth phase of the present invention relates to the optical encoder according to the twenty seventh phase, wherein the optical encoder is configured preferably to satisfy approximately the  
20 relation of  $1/z_1 + 1/z_2 = \lambda / (n(p_1)^2)$ , where  $z_1$  is a distance between the light source unit and the scale,  $z_2$  is a distance between the scale and the light detector,  $p_1$  is a pitch of the periodic optical pattern of the scale,  $\lambda$  is a wavelength of the light beam  
25 emitted from the light source unit, and  $n$  is an integer.

The thirtieth phase of the present invention

relates to the optical encoder according to the twenty seventh phase, wherein the optical element which sets a beam divergent angle of the light beam to a predetermined value is preferably a lens.

5           The thirty first phase of the present invention relates to the optical encoder according to the thirtieth phase, wherein the lens is preferably a concave lens.

10           The thirty second phase of the present invention relates to the optical encoder according to the thirtieth phase, wherein the lens is preferably an optical system composed of a lens group.

15           The thirty third phase of the present invention relates to the optical encoder according to the thirtieth phase, wherein the lens is preferably a cylindrical lens having a focusing action only in the scale moving direction.

20           The thirty fourth phase of the present invention relates to the optical encoder according to the thirtieth phase, wherein the lens has preferably a function of expanding the beam divergent angle of the light beam lens in the scale moving direction, and has a function of focusing the beam divergent angle of the light beam in a plane orthogonal to the scale moving direction and parallel to the scale pattern, .

25

          The thirty fifth phase of the present invention relates to the optical encoder according to the

thirtieth phase, wherein the optical element which sets a beam divergent angle of the light beam to a predetermined value is disposed preferably such that the light beam emitted from the light source unit is reflected by the scale, and then does not shield an optical path from the scale toward a region of the light detector having an effective optical sensitivity.

The thirty sixth phase of the present invention relates to the optical encoder according to the thirtieth phase, preferably further comprising a plurality of photo detectors which detect a predetermined phase portion of the light intensity pattern on a receiving surface of the light detector formed when the light beam emitted from the light source unit and traveled by way of the scale impinges upon the receiving surface.

The thirty seventh phase of the present invention relates to the optical encoder according to the thirtieth phase, the photo detector of the light detector is configured preferably to be capable of detecting a predetermined phase portion of a light intensity pattern formed on the receiving surface of the light detector of which period  $p_2$  is about  $(z_2 + z_3)/z_3 \times p_1$ , where  $z_2$  is a distance between the scale and the light detector,  $p_1$  is a pitch of the periodic optical pattern of the scale, and  $z_3$  is a distance from a position of a virtual spot light source to the scale, the position being calculated from the divergent angle



of the light beam having passes through the optical element which sets a beam divergent angle of the light beam to a predetermined value.

5 The thirty eighth phase of the present invention relates to the optical encoder according to a method of adjusting a level of an output signal depending on a period  $p_2$  of a light intensity pattern formed on a receiving surface of a light detector, in an optical encoder comprising: a light source unit; a scale  
10 which has a periodic optical pattern and displaces relatively to the light source unit; and a light detector to detect a light beam emitted from the light source unit and traveled by way of the scale, the method comprising:

15 (i) a step of setting a beam divergent angle of a light beam emitted from a light source of the light source unit to a predetermined value;

(ii) a step of calculating a position of a virtual spot light source from the set beam divergent angle;

20 (iii) a step of detecting a light intensity pattern formed on the surface of the light detector;

(iv) a step of checking the level of the output signal depending on the period  $p_2$  of the light intensity pattern detected by the light detector;

25 (v) a step of determining whether or not the level of the output signal is included in a predetermined range; and

(vi) a step of terminating the adjustment when the level of the output signal is included in the predetermined range of the output signal, and changing the distance from the calculated position of the virtual spot light source to the scale when the level of the output signal is not included in the predetermined range of the signal level,

wherein the steps from (iii) to (vi) are repeated to adjust the output signal level.

The thirty ninth phase of the present invention relates to an optical encoder comprising:

a light source unit;

a scale which has a periodic optical pattern and dislocates relatively to the light source unit; and

a light detector to detect a light beam emitted from a light source of the light source unit and traveled by way of the scale;

wherein the light source unit has a light beam exit opening through which a light beam is emitted toward the scale, and

the width  $W$  of the light beam exit opening in the scale moving direction is determined depending on the value of  $p_1 \times (z_1 + z_2)/z_2$ , where  $z_1$  is a distance between the light beam exit opening and the scale,  $z_2$  is a distance between the scale and the light detector, and  $p_1$  is a pitch of the periodic optical pattern of the scale.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWING

The accompanying drawings, which are incorporated in and constitute a part of the specification, illustrate presently preferred embodiments of the invention, and together with the general description given above and the detailed description of the preferred embodiments given below, serve to explain the principles of the invention.

FIG. 1 is a diagram showing a configuration of an optical encoder according to a first embodiment of the invention.

FIG. 2 is a diagram showing a configuration of a light detector 3 according to the first embodiment.

FIG. 3 is a diagram showing a configuration of a reflection type optical encoder as a modified example of the first embodiment.

FIG. 4 is a diagram showing a current confinement type LED having a light beam exit window width  $W_L$ s for use in a second embodiment of the invention.

FIG. 5 is a diagram showing the opening width  $W_s$  in the second embodiment.

FIG. 6 is a diagram explaining a Talbot image without slits 100, using a coherent light source 1 having a light beam exit window width  $W_L$ s larger than a slit pitch  $p_1$ .

FIG. 7 is a diagram for general explanation of a Talbot image.

FIG. 8 is a diagram showing a configuration in which plural rows of slit openings 102 arranged at pitch  $p_s$  according to a third embodiment of the invention.

5           FIG. 9 is a diagram showing overlapping of Talbot images formed by light beams emitted from two slits apart at distance  $p_s$ .

FIGS. 10A and 10B are diagrams showing an example of the shape of the slit openings 102.

10           FIGS. 11A and 11B are diagrams showing another example of the shape of the slit openings 102.

FIG. 12 is a diagram explaining a method of adjusting a level of an output signal of a light detector depending on a period  $p_2$  of a light intensity pattern formed on a receiving surface of a light  
15           detector.

FIG. 13 is a diagram showing a configuration of an optical encoder according to a fifth embodiment of the invention.

20           FIG. 14 is a diagram showing a configuration of a reflection type optical encoder as a modified example of the fifth embodiment.

FIG. 15 is a diagram showing the vicinity of a light source 1 of an optical encoder according to  
25           a sixth embodiment of the invention.

FIG. 16 is a diagram showing a bar lens having a lens function only in one axial direction according

to a seventh embodiment of the invention.

FIGS. 17A and 17B are diagrams explaining the action of the bar lens shown in FIG. 16.

FIG. 18 is a diagram showing a cylindrical lens acting as a concave lens in one direction and acting as a convex lens in a direction orthogonal thereto.

FIGS. 19A and 19B are diagrams explaining the action of the cylindrical lens shown in FIG. 18.

FIG. 20 is a diagram showing a configuration of an optical encoder according to an eighth embodiment of the invention.

FIGS. 21A and 21B are diagrams showing a modified example of the light beam emitted from the light source 1.

FIG. 22 is a diagram explaining an adjusting method according to a ninth embodiment of the invention.

FIG. 23 is a diagram showing a configuration of a typical optical encoder in a prior art.

FIG. 24 is a diagram showing a waveform of a detection signal showing the moving distance of a scale.

FIG. 25 is a diagram explaining a Talbot image.

#### DETAILED DESCRIPTION OF THE INVENTION

An outline of an optical encoder of the invention is explained in the first place. A sensor head of the optical encoder of the invention uses a coherent light

source having a light beam exit window width satisfying the condition calculated from a pitch of a scale, a distance between a light source and the scale, and a distance between the scale and a light detector, and is therefore designed to obtain a sufficient contrast of a light intensity pattern projected on the light detector. The coherent light source having a light beam exit window width smaller than the scale pitch is not always required.

The sensor head of the optical encoder of the invention has an optical element for transmitting a predetermined portion of the light beam emitted from the light source, disposed between the light source and the scale. Therefore, a light intensity pattern of large contrast is formed even in the case of using the scale of a small scale pitch for the width of the light source, and by detecting it, the scale of a smaller scale pitch is realized as compared with the light beam exit window width of the light source.

Further, the optical encoder of the invention has an optical element for transmitting a predetermined portion of the light beam emitted from the light source, disposed between the light source and the scale, or has an optical element for setting a beam divergent angle of the light beam emitted from the light source at a predetermined value, and thereby the magnification factor of the Talbot image can be

adjusted. Therefore, it is not required to reduce the width of a photo diode for composing the photo detector, so that the scale of a smaller scale pitch can be used. In addition, even if the same scale is  
5 used, since the Talbot image is magnified, the resolution can be further enhanced.

Referring now to the drawings, the optical encoder of the invention is more specifically described below.  
(First embodiment)

10 FIG. 1 is a diagram showing a configuration of an optical encoder according to a first embodiment of the invention, which comprises a light source 1, a scale 2 having a periodic optical pattern relatively and displacing to the light source 1, and a light detector  
15 3 for detecting the light beam emitted from the light source 1 and passing through the scale 2. Slits 100 are provided between the light source 1 and the scale 2, and the light source 1 and the slits 100 compose a light source unit 10.

20 The light source 1 is an LED which emits a light beam of wavelength  $\lambda$ , and the scale 2 is a transmission type scale having a scale pitch  $p_1$ . The slits 100 are slits having a slit opening 102 in a substantially same size as the scale pitch  $p_1$ .

25 The light beam emitted from the light source 1 is directed toward the slits 100, and only the light beam having passes through the slit opening 102 is emitted

toward the scale 2. At this time, the light beam having passed through the slit opening 102 is emitted toward the scale 2 as a spherical wave on a virtual spot light source of the slit opening 102, and enters  
5 the light detector 3 by way of the scale 2.

FIG. 2 is a diagram showing a configuration of the light detector 3 of the embodiment, which is composed of a photo detector array in which a plurality of photo detector 4 are arranged one-dimensionally. The photo  
10 detector array is divided into four groups, +A, +B, -A, and -B, each connected electrically in every period of  $p20$ , so as to detect four phase portions different in phase by 90 degrees each of the light and dark pattern having period of  $p2$ . Signals to be detected by the  
15 four groups are four signals differing in phase by 90 degrees each, and, for example, (+A) and (-A) are inverted signals different in phase by 180 degrees. The phase A signal and phase B signal in FIG. 25 are outputted as phase A signal = (+A) - (-A), and phase B  
20 signal = (+B) - (-B).

It is known that a Talbot image is formed on the light detector 3 when the light source 1, scale 2, and light detector 3 are in the positional relation as defined in the above formula (1). In this embodiment,  
25 since the slit opening 102 of the slits 100 can be regarded as a virtual light source position, as far as the slit opening 102, scale 2, and light detector 3 are



disposed in the relation in the formula (1), a Talbot image is formed on the light detector 3. In this case, the formula (1) may be expressed as follow:

$$(1/z_1) + (1/z_2) = \lambda / (k(p_1)^2) \quad (1')$$

5 where  $z_1$  is a distance between the slit opening 102 and the surface on the scale 2 having the diffraction grating formed thereon;

$z_2$  is a distance between a surface on the scale 2 having diffraction grating formed thereon and the light  
10 detector 3;

$p_1$  is a pitch of the diffraction grating on the scale 2;

$\lambda$  is a wavelength of a light beam emitted from the light source 1; and

15  $k$  is a natural number.

A pitch  $p_2'$  of a diffraction interference pattern of the Talbot image projected on the light detector 3 in the embodiment is similarly calculated as follows on the basis of the above formula (2):

$$20 \quad p_2' = p_1(z_1 + z_2)/z_1 \quad (2')$$

where  $p_2'$  is a pitch of a diffraction interference pattern on the receiving surface of the light detector 3; and

$p_{20}$  is a pitch of a photo detector array formed on  
25 the light detector 3, that can detect the diffraction interference pattern.

Therefore, by setting the relation of  $p_{20}$  and  $p_2'$

as shown in the following formula (3), the light detector 3 can detect the motion of the Talbot image.

$$P20 = p2' = p1(z1 + z2)/z1 \quad (3)$$

5 In this configuration, even in the case of using the light source having a large light beam exit window as compared with the scale pitch, a Talbot image having a sufficient contrast can be projected on the light detector, and further by adjusting the position of the slits 100, the magnification factor of the Talbot  
10 image can be adjusted without changing the position of the light source 1 and light detector 3. Therefore, without increasing the cost practically, the scale 2 of small pitch can be used, and even if the pitch of the photo detectors is the same, an optical encoder of  
15 higher resolution can be composed.

In the embodiment, the transmission type optical encoder is explained. However, as shown in FIG. 3, substantially the same configuration can be applied in a reflection type optical encoder in which the light  
20 beam emitted from the light source 1 is reflected by the scale 20, and the reflected beam is detected by the light detector 3 disposed at the same side as the light source 1. Reference numeral 35 is a photo detector of the light detector 3.

25 Thus, in the reflection type optical encoder, the light beam reflected by the scale 20 enters a portion having an effective optical sensitivity of the photo

detector 35 formed on the light detector 3, and it is preferred that the slits 100 does not shield a path of the light beam which travels from this scale 20 toward the photo detector 35 formed on the light detector 3.

5 (Second embodiment)

An optical encoder according to a second embodiment of the invention is explained. The configuration and operation of the second embodiment are basically same as in the first embodiment described by reference to FIG. 1, and the detailed description of the configuration is omitted herein. The second embodiment is different from the first embodiment in that the light source 1 is a current confinement type LED having a light beam exit window width  $W_L$ s as shown in FIG. 4, and the opening width in the moving direction of the scale 2 of the slit opening 102 is an effective opening width  $W_s$  (see FIG. 5) as described below.

As compared with the ordinary LED which emits light from the entire surface of the LED, since the current confinement type LED emits light only in a specified area, the light intensity per unit solid angle is large. Therefore, when it is desired to illuminate the scale by the light beam of the same optical intensity, a smaller power is realized, so that the optical encoder can be operated more efficiently.

In this embodiment, the slits 100, scale 2, and

light detector 3 are disposed such that  $z_1$  and  $z_2$  are equal to each other in formula (1'). Therefore, from formula (2'),  $p_2' = p_{20} = 2 \times p_1$  is obtained.

5 The light beam exit window width  $W_L$ s of the light source 1 is larger than the scale pitch  $p_1$  of the scale 2, whereas the opening width  $W_s$  of the slit opening 102 is odd-number times of the scale pitch  $p_1$ .

Using the light source 1 of which light beam exit window width  $W_L$ s is larger than the slit pitch  $p_1$ , the  
10 Talbot image without using the slits 100 is explained by referring to FIG. 6.

When the light source 1 has the light beam exit window width  $W_L$ s, it may be supposed that a plurality of spot light beams are positioned on the exit window.  
15 FIG. 6 shows a Talbot image by two spot light sources 1-L and 1-R spaced from each other by distance  $p_1$  on the exit window of the light source 1. As shown in FIG. 6, the light portion of a Talbot image 7-R by the spot light source 1-R and the dark portion of a Talbot  
20 image 7-L by the spot light source 1-L are overlapped, and the dark portion of the Talbot image 7-R by the spot light source 1-R and the light portion of the Talbot image 7-L by the spot light source 1-L are overlapped. As a result, the Talbot images by the both  
25 spot light sources 1-L and 1-R cancel each other.

More specifically, when the distance between two virtual spot light sources on the exit window of the

light source 1 is equal to the scale pitch  $p_1$ , they cancel each other, and do not contribute to formation of the Talbot image. Theoretically, when the interval of virtual spot light sources is even-number times of the period  $p_1$  of the light beam, since the spot of interval of  $p_1$  can be found in all spots on the light beam exit window of the light source, the Talbot image is completely deleted. To the contrary, in the case of odd-number times of  $p_1$ , portions which do not cancel Talbot images each other are left over.

In the configuration of the second embodiment of the invention, suppose the slits 100 having the opening width  $W_s$  of odd-number times of the scale pitch  $p_1$  are inserted as shown in FIG. 1. In this case, of the light beams emitted from the light source 1, only the light beam having passed through the slit opening 102 of the slits 100 is directed toward the scale 2. At this time, the slit opening 102 may be regarded as a virtual light source. This slit opening 102 has the width of odd-number times of the scale pitch  $p_1$ . Thus, the plurality of virtual spot light sources for composing the slit opening 102 as the light source has a set of spot light sources not finding the mutually canceling spot light sources by the portion of the width  $p_1$ , even if the spot light sources of mutually canceling Talbot images are deleted. Therefore, a Talbot image of a sufficient contrast can be formed.

Incidentally, the light beams which do not contribute to formation of the Talbot image by canceling each other enter the light detector 3 as background light, which adds to the background of the detection signal, and it causes to lower the relative contrast of the Talbot image detected by the light detector 3. When the light beam exit window width  $W_L$  is sufficiently large as compared with the scale pitch  $p_1$ , since the background becomes high as mentioned above, the contrast of the diffraction interference pattern of the Talbot image detected by the light detector 3 to be smaller, and it is not a preferred configuration. Practically, by setting the opening width  $W_s$  of the slit opening 102 at several times of the scale pitch  $p_1$ , a diffraction interference pattern of the Talbot image of large contrast can be formed.

On the other hand, when the light beam emitted from the light source 1 is small in the intensity in the peripheral area as compared with that on the optical axis as in the case of the light source having a beam profile conforming to, for example, Gaussian distribution, the light beams passing through the slits 100 are not always uniform, but distribute in light intensity. Accordingly, when the opening width  $W_s$  of the slit opening 102 is slightly larger than two times the scale pitch  $p_1$ , the contrast of the Talbot image is the minimum.

In this embodiment,  $z_1$  and  $z_2$  are equal in the formula (1'), that is, the pitch  $p_2'$  of the Talbot image is two times the scale pitch  $p_1$ , and a more general explanation is given in FIG. 7.

5           The light beams emitted from the virtual spot light sources on the light beam exit window of the light source 1 illuminate the scale 2, and a Talbot image is formed on the receiving surface of the light detector 3. FIG. 7 shows the position of the light  
10           and dark pattern of the Talbot image formed on the receiving surface of the light detector 3 when the scale 2 is fixed on the light source 1. The light beam emitted from a certain spot passes through an opening on the scale 2, and reaches the receiving surface  
15           of the light detector 3. At this time, when the wavelength of the light source 1, the distance  $z_1$  between the slits 100 and the scale 2, the distance  $z_2$  between the scale 2 and the light detector 3, and the pitch  $p_1$  of the scale 2 satisfy the relation of the  
20           formula (1'), a Talbot image is formed on the receiving surface of the light detector 3.

          An emitting light beam from a certain point P on the slit opening 102 passes through a certain opening on the scale 2, and forms a peak of a Talbot image on  
25           a point T on the receiving surface of the light detector 3. The pitch  $p_2'$  of the Talbot image by this spot light source P is the pitch calculated by the

formula (2')), and a light and dark pattern is formed periodically on the receiving surface of the light detector 3 as shown in the diagram. Next, suppose an emitting light beam from a light source P' apart from this light source P by distance W2 passes through the same opening on the scale 2, and reaches a position T' of the peak next to the Talbot image formed by the light source P of the Talbot image formed on the light detector 3. The Talbot images formed by the light source P and light source P' completely overlap each other, and emphasize each other. At this time, the relation is as shown in formula (4).

$$W2 = P2' \times z1/z2 = p1 \times (z1+z2)/z2 \quad (4)$$

Suppose a position of the light source 1 for forming a peak of the Talbot image somewhere between the point T and the point T'. As clear from FIG. 7, such position P" of the light source 1 is an intermediate position between point P and point P'. That is, W1 in the diagram is given in the following formula.

$$\begin{aligned} W1 &= W2/2 = P2' \times z1/(2 \times z2) \\ &= p1 \times (z1 + z2)/(2 \times z2) \end{aligned} \quad (5)$$

That is, in a more general case of the embodiment, the opening width Ws of the slit opening 102 may be defined in the following range.

$$p1 \times (z1 + z2)/(2 \times z2) \times (2n - 1.5) \leq Ws \leq p1 \times (z1 + z2)/(2 \times z2) \times (2n - 0.5) \quad (6)$$



where  $n$  is a natural number.

If  $W_s$  is out of the range of the formula (6), the signal level deteriorates, but does not deteriorate immediately to an impractical level. Therefore,  
5 preferably,  $W_s$  is in the range of the formula (6), but its function is not lost immediately even if slightly going out of the range. Hence, it is sufficient that  $W_s$  is approximately included in this range.

As in this embodiment, if the case of  $z_2 = z_1$ ,  
10 the formula (6) is rewritten as follows:

$$p_1 \times (2n - 1.5) \leq W_s \leq p_1 \times (2n - 0.5) \quad (6')$$

In such configuration, a Talbot image of a larger contrast can be formed, and the output signal from the light detector 3 may be also a signal of high  
15 intensity.

In this embodiment, the slit opening 102 is shown as an example of square slits 100, but it may be also formed as circular, elliptical, quadrangular, polygonal and the like as far as not departing from the true  
20 spirit and the scope of the invention.

(Third embodiment)

An optical encoder according to a third embodiment of the invention is explained. The configuration and operation of the third embodiment are basically same  
25 as in the first embodiment described by reference to FIG. 1, and the detailed description of the configuration is omitted herein. The third embodiment is

different from the first embodiment in that the light source 1 is a current confinement type LED having a light beam exit window width  $W_L$ s as shown in FIG. 4, and the slit opening 102 of the slits 100 is composed of a plurality of slit openings (see FIG. 8) arranged at slit pitch  $p_s$ .

In this embodiment, the slit pitch  $p_s$  of the slit openings 102 is about integer times of the scale pitch  $p_1$ , and is set at about integer times of the pitch  $p_2$  of the Talbot images.

FIG. 9 shows an overlapping image of Talbot images formed by light beams emitted from two slits apart from each other by slit pitch  $p_s$ . As shown in FIG. 9, by setting the slit pitch  $p_s$  about integer times of the scale pitch  $p_1$  and about integer times of the pitch  $p_2$  of the Talbot images, the diffraction interference patterns of a Talbot image 7-R formed by a light beam having passed through a slit opening 102-R, and a Talbot image 7-L formed by a light beam having passed through the slit opening 102-L overlap each other, and a Talbot image of a higher light intensity can be formed on the light detector 3.

Incidentally, when  $z_1$  and  $z_2$  are nearly equal to each other, it is known from the formulas (1') and (2') that the slit pitch  $p_s$  be about integer times of the pitch  $p_2$  of the Talbot images, that is, about even-number times of  $p_1$ .

More generally, it is sufficient that the slits 100 are disposed at positions of integer times of  $W_2$  shown in the formula (4), that is, the openings 102 of the slits 100 are disposed at positions of  $n \times (z_1 + z_2)/z_2$  times of the pitch  $p_1$  of the scale 2 where  $n$  is a natural number.

In FIG. 8, four slit openings 102 are provided, but the number is not particularly specified as far as it is two or more, and the shape of the slit openings 102 may be modified freely as shown in FIGS. 10A and 10B, including a circular shape of the slit opening 102 (FIG. 10A), square, polygonal, elliptical or other shapes. Other modifications include two-dimensional layout as shown in FIG. 10B, layout according to the shape of the beam spots 104 on the slits 100 by the light beam emitted from the light source 1 (FIGS. 11A and 11B), and the like.

The slits 100 include a type having through-holes formed in a shielding member made of a metal or the like, a type in which a metal film formed on a glass plate is patterned by etching or other technique, or any other type using a member allowing to transmit a predetermined portion of light beam.

In the configuration of the embodiment, by effectively making use of the light beams emitted from the light source 1 without increasing the intensity of the light beams emitted from the light source 1,

the light intensity of the Talbot image entering the light detector 3 can be enhanced.

(Fourth embodiment)

A fourth embodiment of the invention is explained.

5 The fourth embodiment of the invention relates to a method of adjusting a level of an output signal of a light detector depending on a period  $p_2$  of a light intensity pattern formed on a receiving surface of the light detector. FIG. 12 is a flowchart explaining the  
10 detail of such an adjusting method. First, a light intensity pattern formed on the receiving surface of the light detector is detected (step S1). Next is detected a level of an output signal corresponding to a period  $p_2$  of the light intensity pattern outputted  
15 from the light detector (step S2). The detected level of the output signal is determined to be included in a predetermined range or not (step S3). If determination is No, by changing a position of an optical element relatively to the scale and light detector, the  
20 distance is changed from a virtual spot light source to the scale, and the position of the optical element is adjusted (step S4), and back to step S1, the same process is repeated. The process is stopped when determination is Yes in step S3.

25 Herein, the light detector is configured to detect a light intensity pattern having a preset specific period ( $p_{20}$ ). Therefore, if the period  $p_2$  is different

from the preset period p20, the efficient detection is impossible, and as a result, the level of the output signal is lowered. Thus, by adjusting the position of the optical element in step S4, the level of the output  
5 signal can be improved.

(Fifth embodiment)

A fifth embodiment of the invention is explained. FIG. 13 is a diagram showing an optical encoder in the fifth embodiment of the invention. The optical encoder  
10 shown in FIG. 13 is a transmission type optical encoder, and is characterized by disposing a light source 1 and a concave lens 200 as a light source unit 10. The light source 1 is a current confinement type LED which emits a light beam in wavelength of  $\lambda$ , and  
15 a scale 2 is a scale having a scale pitch p1, and the concave lens 200 is an optical element for adjusting a beam divergent angle of the light beam emitted from the light source 1 to a specified angle.

The light beam emitted from the light source 1 is  
20 directed toward the concave lens 200, and this light beam passes through the concave lens 200, and is emitted toward the scale 2. At this time, the light beam having passed through the concave lens 200 is expanded in its beam divergent angle by this concave  
25 lens 200, and it may be assumed that the light source is present at a virtual spot light source position 202 indicated by X. It is known that the Talbot image is

formed on the light detector 3 when the positions of the light source 1, scale 2 and light detector 3 are in a specified relation as shown in the formula (1). This Talbot image forms a diffraction interference pattern depending on the phase difference in every path of the light beam when the light beam emitted from the light source 1 reaches onto the light detector 3. Therefore, when the concave lens 200 is inserted in the path of the light beam, approximately, the positional relation of the light source 1, scale 2 and light detector 3 is assumed to be unchanged although it is required to calculate the distance between the light source 1 and the scale 2 in the path of the light beam having passed through the concave lens 200, such as the diffractive index and diffraction angle of the concave lens 200. Practically, by disposing the light source 1, scale 2 and light detector 3 without using the concave lens 200, the positional relation of the members may be adjusted as required on the basis of the output signal from the light detector 3.

On the other hand, the pitch of the diffraction interference pattern of the Talbot image projected on the light detector 3 is calculated according to the formula (2) from the positional relation of the spot light source, scale and light detector because the light beam emitted from the spot light source passes through the slits and forms a light pattern or a dark

pattern at position projected on the light detector 3.  
In this embodiment, since the position of the virtual  
spot light source is the position indicated by 202 in  
FIG. 13, it is determined in the following formula (7):

5           
$$P2'' = p1(z2 + z3)/z3 \quad (7)$$

where  $z3$  is a distance between the virtual spot light  
source position 202 by the concave lens 200 and the  
surface on the scale 2 having the diffraction grating  
formed thereon, and the virtual spot light source  
10 position 200 generally means a back focal point of the  
concave lens 200;

$p2''$  is a pitch of a diffraction interference  
pattern of the Talbot image projected on light detector  
3 in the case where the concave lens 200 is provided;  
15 and

other parameters are same as in the first  
embodiment.

In this configuration, the magnification factor of  
the Talbot image can be changed without changing the  
20 positional relation of the light source 1, scale 2 and  
light detector 3. Further, the scale 2 of smaller  
pitch can be used, or an optical encoder of higher  
resolution can be composed at the same pitch of the  
light detector.

25           In this embodiment, the case in which the concave  
lens 200 is used is described. However, the same  
effects can be obtained by using a convex lens having

the back focal point of the lens located somewhere between the light source 1 and the scale 2.

The transmission type optical encoder is explained in the embodiment. However, as shown in FIG. 14, the same configuration is realized in a reflection type optical encoder designed to reflect the light beam emitted from the light source 1 by the scale 20 and detect the reflected beam by the light detector 3 disposed at the same side as the light source 1. Reference numeral 35 is a photo detector 35 of the light detector 3.

Thus, in the reflection type optical encoder, the light beam from the scale 20 enters the portion having an effective optical sensitivity of the photo detector 35 formed on the light detector 3, and it is preferred that the path of this light beam is not shielded by the concave lens 200.

(Sixth embodiment)

A sixth embodiment of the invention is described below. The sixth embodiment is differ from the fifth embodiment shown in FIG. 13 in that the concave lens 200 is replaced by a pair of a convex lens and a concave lens, and other configuration is same as in the fifth embodiment shown in FIG. 13.

FIG. 15 is a diagram showing the vicinity of the light source 1 of the optical encoder according to the sixth embodiment. The light beam emitted from the



light source 1 is transformed into collimated beam by  
a collimator lens 200-1, and is directed toward  
a concave lens 200-2. The collimated beam entering the  
concave lens 200-2 is expanded to a predetermined beam  
5 divergent angle, and is emitted toward the scale 2.  
The subsequent operation is same as in the fifth  
embodiment.

In this configuration, even if the concave lens  
200-2 moves in the arrow direction in the drawing,  
10 the light beam entering the concave lens 200-2 is a  
collimated beam, and hence there is no change. As a  
result, there is no change in the divergent angle of  
the light beam having passed through the concave lens  
200-2 or in intensity distribution of light beam, so  
15 that a much stable light beam is emitted toward the  
scale 2.

By such configuration, even if the beam divergent  
angle of the light source 1 is unstable, the light  
beam divergent angle emitted to the scale 2 is stable,  
20 so that the signal outputted from the light detector 3  
is further improved in stability.

In the embodiment, one concave lens and one convex  
lens are used. However, by using three or more lenses,  
the position of the virtual spot light source 202 may  
25 be adjusted to the scale 2 side from the leading end  
lens, or the phase difference can be adjusted in each  
optical path of the light beam emitted from the light

source 1 until reaching the light detector 3, so that the contrast of the Talbot image may be further enhanced.

(Seventh embodiment)

5           A seventh embodiment of the invention is described. The seventh embodiment is different from the fifth embodiment in that the concave lens of the optical encoder in the fifth embodiment shown in FIG. 13 is a bar lens having a lens function only in  
10           one axial direction as shown in FIG. 16, and other aspects are same as in the fifth embodiment explained in FIG. 13.

          A lens 200-3 shown in FIG. 16 is a bar concave lens having a lens function in the moving direction  
15           of the scale 2, but not having a lens function in a direction orthogonal to the moving direction of the scale 2 in a plane parallel to the pattern surface of the scale 2.

          In this configuration, as shown in FIGS. 17A and  
20           17B, since the light beam emitted from the light source 1 is expanded to a desired beam divergent angle in the scale moving direction by the lens 200-3, the magnification factor of the diffraction interference pattern of the Talbot image projected on the light  
25           detector 3 can be set to a predetermined value. In the direction orthogonal to the moving direction of the scale 2 in the plane parallel to the pattern surface of

the scale 2, since the beam divergent angle is not expanded, the beam intensity of the light beam entering the photo detector 4 on the light detector 3 is not lowered, so that a sufficient intensity can be obtained  
5 in the signal detected by the light detector 3.

This embodiment uses the cylindrical lens having a lens function in one direction but not having a lens function in a direction orthogonal thereto. However, it is also possible to use a cylindrical lens 200-4  
10 acting as a concave lens in one direction and acting as a convex lens in a direction orthogonal to the one direction as shown in FIGS. 18, 19A and 19B. In this configuration, without spoiling the function of the embodiment, in the direction orthogonal to the moving  
15 direction of the scale 2 in the plane parallel to the pattern surface of the scale 2, the light beam can be focused and entered in the photo detector 4 on the light detector 3, so that the signal intensity detected by the light detector 3 can be further enhanced.

20 (Eighth embodiment)

An eighth embodiment of the invention is described below. FIG. 20 is a diagram showing a configuration of an optical encoder according to the eighth embodiment of the invention. This embodiment is different from  
25 the first embodiment in that a light source unit 10 has a light source 1, slits 100, and a collimating lens 200-5, but other aspects are same as in the first

embodiment.

In this embodiment, the light beam emitted from the light source 1 is transformed into collimated beam by the collimating lens 200-5. The collimated beam is emitted to the slits 100, and the light beam having passed through the opening 102 of the slits 100 is emitted toward the scale 2. At this time, the position of the virtual spot light source coincides with the slit opening 102.

In the embodiment, since the light beam emitted from the light source is transformed into collimated beam by the lens 200-5, even if the slits 100 are moved in the vertical direction in the diagram, the intensity of the light beam passing through the slit opening 102 is constant. Accordingly, even if the slits 100 are moved, the light intensity of the Talbot image detected by the light detector 3 is not changed.

Therefore, by composing as in the embodiment, even in the case where the magnification factor of the Talbot image formed on the light detector 3 is adjusted by moving the slits 100 in the vertical direction in the diagram, the light intensity of the Talbot image detected by the photo detector 4 of the light detector 3 is constant, so that the magnification factor can be adjusted more stably.

In the embodiment, the light beam emitted from the light source 1 is transformed into collimated beam

by using the lens 200-5. However, as shown in FIG. 21A, by composing so as to focus in the vicinity of the slit opening 102, the light intensity of the Talbot image detected by the light detector 3 can be increased. Further, as shown in FIG. 21B, by slightly reducing the collimated beam shape, the adjustment allowance of the slits 100 can be increased, and the light intensity of the Talbot image can be increased at the same time.

(Ninth embodiment)

A ninth embodiment of the invention is described. The ninth embodiment of the invention is basically same as the configuration shown in FIG. 25, except that the light source 1 herein is a current confinement type LED having a light beam exit window width WLs as shown in FIG. 4. The light beam exit window width WLs is defined in the following range according to the formula (6).

$$P1 \times (2n - 1.5) \times \frac{z1 + z2}{2z2} \leq WLs \leq P1 \times (2n - 0.5) \times \frac{z1 + z2}{2z2} \quad (8)$$

In this configuration, the light beam exit window width WLs of the light source 1 is not always required to be smaller than the scale pitch p1, and even when the same light source 1 is used, it is applicable to the scale 2 having a scale pitch p1 in a wide range satisfying the above formula (8).

In the case of  $z1 = z2$ , the formula (8) can be rewritten as follows.

$$p_1 \times (2n - 1.5) \leq W_L \leq p_1 \times (2n - 0.5) \quad (8')$$

Further, by defining the light beam exit window width  $W_L$  in the moving direction of the scale 2 at  $p_1 \times (z_1 + z_2)/(2 \times z_2)$  or less, or at about  $p_1 \times$   
5  $(2n - 1) \times (z_1 + z_2)/(2 \times z_2)$ , a Talbot image of higher contrast can be formed.

Herein, if  $W_L$  is out of the range of the formula (8), the signal level deteriorates, but does not deteriorate immediately to an impractical level.  
10 Therefore, preferably,  $W_L$  is in the range of the formula (8), but its function is not lost immediately even if slightly going out of the range. Hence, it is sufficient that  $W_L$  is approximately included in this range.

15 In the embodiment, the light source may be a semiconductor laser of surface emission type, and the same effects can be obtained.

Further, by using the light emitting element having plural light beam exit windows at positions of  
20  $(z_1 + z_2)/z_2 \times n$  times of the scale pitch  $p_1$ , a Talbot image of a much larger contrast can be obtained. In particular, it is easier to fabricate an array in the LED, surface-emitting laser, and other surface-emitting elements, and it is particularly preferred  
25 because the positional relation of the light beam exit windows can be fabricated correctly.

(Tenth embodiment)

A tenth embodiment of the invention is described. The tenth embodiment of the invention relates to a method of adjusting a level of an output signal of a light detector depending on a period  $p_2$  of a diffraction interference pattern by using an optical element for setting a beam divergent angle of a light beam emitted from a light source to a predetermined value. FIG. 22 is a flowchart explaining the detail of such an adjusting method. First, a beam divergent angle of a light beam from a light source is set to a predetermined value (step S10). More specifically, an optical element for setting a specified beam divergent angle is selected (step S10-1). The selected optical element is placed between the light source and the scale (step S10-2). From the set beam divergent angle, a position of a virtual spot light source is calculated (step S11). A diffraction interference pattern formed on a receiving surface of a light detector is detected (step S12). Next, a signal level of an output signal is detected depending on a period  $p_2$  of the diffraction interference pattern outputted from the light detector (step S13). Thereafter, the signal level of the detected output signal is determined to be included in a predetermined range or not (step S14). If determination is No, by changing a position of the optical element relating to the scale and light

detector, the distance from the position of the virtual spot light source to the scale is changed, and the position of the optical element is adjusted (step S15), and back to step S10, the same process is repeated.

5 When determination is Yes in step S14, the process is stopped.

In all foregoing embodiments described herein, the interference light source may be realized by a surface-emitting laser, a stripe type semiconductor  
10 laser, a current confinement type LED, an ordinary LED, and any other coherent light source.

In several embodiments of the invention, the slits 100 and the light beam exit window of the light source 1 are disposed apart from each other at a specific  
15 distance, but the slits 100 may be in contact with the exit window of the light source, or may be formed by patterning an upper electrode of the light source or the like.

The lens shown in the embodiments of the invention  
20 includes a general lens shaped from glass or plastics, a Fresnel type diffractive lens, and the like.

Additional advantages and modifications will readily occur to those skilled in the art. Therefore, the invention in its broader aspects is not limited to  
25 the specific details and representative embodiments shown and described herein. Accordingly, various modifications may be made without departing from the



spirit or scope of the general inventive concept as defined by the appended claims and their equivalents.